



**HAMMETT & EDISON, INC.**  
CONSULTING ENGINEERS  
RADIO AND TELEVISION

WILLIAM F. HAMMETT, P.E.  
DANE E. ERICKSEN, P.E.  
STANLEY SALEK, P.E.  
MARK D. NEUMANN, P.E.  
ROBERT P. SMITH, JR.  
RAJAT MATHUR, P.E.  
FERNANDO DIZON  
ROBERT L. HAMMETT, P.E.  
1920-2002  
EDWARD EDISON, P.E.

BY E-MAIL [DDOMRESE@SBASITE.COM](mailto:DDOMRESE@SBASITE.COM)

August 24, 2009

Mr. David Domrese  
New Tower Development  
SBA Network Services, Inc.  
5900 Broken Sound Parkway, N.W.  
Boca Raton, Florida 33487

Dear Dave:

As you requested, we have analyzed the RF exposure conditions near the SBA Network Services, Inc. project (Site No. CA1142-S) located at Grouse Drive and Chukar Circle in Homewood, California. An electronic copy of our report is enclosed. Fields in publicly accessible areas at the site are calculated to be well below the applicable limits.

We appreciate the opportunity to be of service and would welcome any questions on this material. Please let me know if we may be of additional assistance.

Sincerely yours,

William F. Hammett

tm

Enclosure

cc: Mr. Steve Christenson (w/encl) – BY E-MAIL [STEVECHRJSTENSON@SBCGLOBAL.NET](mailto:STEVECHRJSTENSON@SBCGLOBAL.NET)

**SBA Network Services, Inc. • New Radio Tower (Site No. CA1142-S)  
Grouse Drive and Chukar Circle • Homewood, California**

about 1 inch thick. Because of the short wavelength of the frequencies assigned by the FCC for wireless services, the antennas require line-of-sight paths for their signals to propagate well and so are installed at some height above ground. The antennas are designed to concentrate their energy toward the horizon, with very little energy wasted toward the sky or the ground. Along with the low power of such facilities, this means that it is generally not possible for exposure conditions to approach the maximum permissible exposure limits without being physically very near the antennas.

**Computer Modeling Method**

The FCC provides direction for determining compliance in its Office of Engineering and Technology Bulletin No. 65, "Evaluating Compliance with FCC-Specified Guidelines for Human Exposure to Radio Frequency Radiation," dated August 1997. Figure 2 attached describes the calculation methodologies, reflecting the facts that a directional antenna's radiation pattern is not fully formed at locations very close by (the "near-field" effect) and that at greater distances the power level from an energy source decreases with the square of the distance from it (the "inverse square law"). The conservative nature of this method for evaluating exposure conditions has been verified by numerous field tests.

**Site and Facility Description**

Based upon information provided by SBA Network Services, it is proposed to install directional panel antennas for use by two wireless telecommunications carriers on a new 140-foot pole, configured to resemble a pine tree, recently constructed by the Tahoe City Public Utility District near Grouse Drive and Chukar Circle in Homewood, California. For the limited purpose of this study, transmitting facilities for those carriers are assumed to be as follows:

| <u>Carrier</u> | <u>Service</u> | <u>Maximum ERP</u> | <u>Antenna Model</u> | <u>Height</u> |
|----------------|----------------|--------------------|----------------------|---------------|
| Carrier #1     | Cellular       | 1,500 watts        | Antel BXA-80040/6    | 110 ft        |
| Carrier #2     | PCS            | 1,500              | Kathrein 742-265     | 75            |
|                | Cellular       | 1,500              |                      |               |

The United States Coast Guard is mounting three Sinclair omnidirectional antennas on the tower, two Model SD214 VHF antennas and one Model SC381 UHF antenna, for transmission at effective heights of 95 and 127 feet above ground, respectively, with a maximum effective radiated power of 560 watts, representing simultaneous operation of four VHF channels at 100 watts each and one UHF channel at 160 watts. The Coast Guard is also installing a receiver-only antenna array at about 143 feet above ground, for direction-finding purposes. There are reported no other wireless telecommunications base stations located nearby.

SBA Network Services, Inc. • New Radio Tower (Site No. CA1142-S)  
Grouse Drive and Chukar Circle • Homewood, California

Authorship

The undersigned author of this statement is a qualified Professional Engineer, holding California Registration Nos. E-13026 and M-20676, which expire on June 30, 2011. This work has been carried out under his direction, and all statements are true and correct of his own knowledge except, where noted, when data has been supplied by others, which data he believes to be correct.

August 24, 2009



*William F. Hammett*  
William F. Hammett, P.E.

## RFR.CALC™ Calculation Methodology

### Assessment by Calculation of Compliance with FCC Exposure Guidelines

The U.S. Congress required (1996 Telecom Act) the Federal Communications Commission (“FCC”) to adopt a nationwide human exposure standard to ensure that its licensees do not, cumulatively, have a significant impact on the environment. The maximum permissible exposure limits adopted by the FCC (see Figure 1) apply for continuous exposures from all sources and are intended to provide a prudent margin of safety for all persons, regardless of age, gender, size, or health. Higher levels are allowed for short periods of time, such that total exposure levels averaged over six or thirty minutes, for occupational or public settings, respectively, do not exceed the limits.

#### Near Field.

Prediction methods have been developed for the near field zone of panel (directional) and whip (omnidirectional) antennas, typical at wireless telecommunications base stations, as well as dish (aperture) antennas, typically used for microwave links. The antenna patterns are not fully formed in the near field at these antennas, and the FCC Office of Engineering and Technology Bulletin No. 65 (August 1997) gives suitable formulas for calculating power density within such zones.

For a panel or whip antenna, power density  $S = \frac{180}{\theta_{BW}} \times \frac{0.1 \times P_{net}}{\pi \times D^2 \times h}$ , in mW/cm<sup>2</sup>,

and for an aperture antenna, maximum power density  $S_{max} = \frac{0.1 \times 16 \times \eta \times P_{net}}{\pi \times h^2}$ , in mW/cm<sup>2</sup>,

where  $\theta_{BW}$  = half-power beamwidth of the antenna, in degrees, and

$P_{net}$  = net power input to the antenna, in watts,

$D$  = distance from antenna, in meters,

$h$  = aperture height of the antenna, in meters, and

$\eta$  = aperture efficiency (unitless, typically 0.5-0.8).

The factor of 0.1 in the numerators converts to the desired units of power density.

#### Far Field.

OET-65 gives this formula for calculating power density in the far field of an individual RF source:

power density  $S = \frac{2.56 \times 1.64 \times 100 \times RFF^2 \times ERP}{4 \times \pi \times D^2}$ , in mW/cm<sup>2</sup>,

where ERP = total ERP (all polarizations), in kilowatts,

RFF = relative field factor at the direction to the actual point of calculation, and

$D$  = distance from the center of radiation to the point of calculation, in meters.

The factor of 2.56 accounts for the increase in power density due to ground reflection, assuming a reflection coefficient of 1.6 ( $1.6 \times 1.6 = 2.56$ ). The factor of 1.64 is the gain of a half-wave dipole relative to an isotropic radiator. The factor of 100 in the numerator converts to the desired units of power density. This formula has been built into a proprietary program that calculates, at each location on an arbitrary rectangular grid, the total expected power density from any number of individual radiation sources. The program also allows for the description of uneven terrain in the vicinity, to obtain more accurate projections.



**HAMMETT & EDISON, INC.**  
CONSULTING ENGINEERS  
RADIO AND TELEVISION

WILLIAM F. HAMMETT, P.E.  
DANE E. ERICKSEN, P.E.  
STANLEY SALEK, P.E.  
MARK D. NEUMANN, P.E.  
ROBERT P. SMITH, JR.  
RAJAT MATHUR, P.E.  
FERNANDO DIZON  
ROBERT L. HAMMETT, P.E.  
1920-2002  
EDWARD EDISON, P.E.

BY E-MAIL [DDOMRESE@SBASITE.COM](mailto:DDOMRESE@SBASITE.COM)

August 24, 2009

Mr. David Domrese  
New Tower Development  
SBA Network Services, Inc.  
5900 Broken Sound Parkway, N.W.  
Boca Raton, Florida 33487

Dear Dave:

As you requested, we have analyzed the RF exposure conditions near the SBA Network Services, Inc. project (Site No. CA1142-S) located at Grouse Drive and Chukar Circle in Homewood, California. An electronic copy of our report is enclosed. Fields in publicly accessible areas at the site are calculated to be well below the applicable limits.

We appreciate the opportunity to be of service and would welcome any questions on this material. Please let me know if we may be of additional assistance.

Sincerely yours,

William F. Hammett

tm

Enclosure

cc: Mr. Steve Christenson (w/encl) – BY E-MAIL [STEVECHRISTENSON@SBCGLOBAL.NET](mailto:STEVECHRISTENSON@SBCGLOBAL.NET)

**SBA Network Services, Inc. • New Radio Tower (Site No. CA1142-S)  
Grouse Drive and Chukar Circle • Homewood, California**

**Statement of Hammett & Edison, Inc., Consulting Engineers**

The firm of Hammett & Edison, Inc., Consulting Engineers, has been retained by SBA Network Services, Inc. to evaluate radio operations on a new tower (Site No. CA1142-S) located at Grouse Drive and Chukar Circle in Homewood, California, for compliance with appropriate guidelines limiting human exposure to radio frequency (“RF”) electromagnetic fields.

**Prevailing Exposure Standards**

The U.S. Congress requires that the Federal Communications Commission (“FCC”) evaluate its actions for possible significant impact on the environment. In Docket 93-62, effective October 15, 1997, the FCC adopted the human exposure limits for field strength and power density recommended in Report No. 86, “Biological Effects and Exposure Criteria for Radiofrequency Electromagnetic Fields,” published in 1986 by the Congressionally chartered National Council on Radiation Protection and Measurements (“NCRP”). Separate limits apply for occupational and public exposure conditions, with the latter limits generally five times more restrictive. The more recent standard, developed by the Institute of Electrical and Electronics Engineers and approved as American National Standard ANSI/IEEE C95.1-2006, “Safety Levels with Respect to Human Exposure to Radio Frequency Electromagnetic Fields, 3 kHz to 300 GHz,” includes similar exposure limits. A summary of the FCC’s exposure limits is shown in Figure 1. These limits apply for continuous exposures and are intended to provide a prudent margin of safety for all persons, regardless of age, gender, size, or health.

The most restrictive FCC limit for exposures of unlimited duration to radio frequency energy for several personal wireless services are as follows:

| <u>Personal Wireless Service</u>   | <u>Approx. Frequency</u> | <u>Occupational Limit</u> | <u>Public Limit</u>     |
|------------------------------------|--------------------------|---------------------------|-------------------------|
| Broadband Radio (“BRS”)            | 2,600 MHz                | 5.00 mW/cm <sup>2</sup>   | 1.00 mW/cm <sup>2</sup> |
| Advanced Wireless (“AWS”)          | 2,100                    | 5.00                      | 1.00                    |
| Personal Communication (“PCS”)     | 1,950                    | 5.00                      | 1.00                    |
| Cellular Telephone                 | 870                      | 2.90                      | 0.58                    |
| Specialized Mobile Radio (“SMR”)   | 855                      | 2.85                      | 0.57                    |
| Long Term Evolution (“LTE”)        | 700                      | 2.33                      | 0.47                    |
| [most restrictive frequency range] | 30–300                   | 1.00                      | 0.20                    |

**General Facility Requirements**

Base stations typically consist of two distinct parts: the electronic transceivers (also called “radios” or “channels”) that are connected to the traditional wired telephone lines, and the passive antennas that send the wireless signals created by the radios out to be received by individual subscriber units. The transceivers are often located at ground level and are connected to the antennas by coaxial cables



**SBA Network Services, Inc. • New Radio Tower (Site No. CA1142-S)  
Grouse Drive and Chukar Circle • Homewood, California**

about 1 inch thick. Because of the short wavelength of the frequencies assigned by the FCC for wireless services, the antennas require line-of-sight paths for their signals to propagate well and so are installed at some height above ground. The antennas are designed to concentrate their energy toward the horizon, with very little energy wasted toward the sky or the ground. Along with the low power of such facilities, this means that it is generally not possible for exposure conditions to approach the maximum permissible exposure limits without being physically very near the antennas.

**Computer Modeling Method**

The FCC provides direction for determining compliance in its Office of Engineering and Technology Bulletin No. 65, "Evaluating Compliance with FCC-Specified Guidelines for Human Exposure to Radio Frequency Radiation," dated August 1997. Figure 2 attached describes the calculation methodologies, reflecting the facts that a directional antenna's radiation pattern is not fully formed at locations very close by (the "near-field" effect) and that at greater distances the power level from an energy source decreases with the square of the distance from it (the "inverse square law"). The conservative nature of this method for evaluating exposure conditions has been verified by numerous field tests.

**Site and Facility Description**

Based upon information provided by SBA Network Services, it is proposed to install directional panel antennas for use by two wireless telecommunications carriers on a new 140-foot pole, configured to resemble a pine tree, recently constructed by the Tahoe City Public Utility District near Grouse Drive and Chukar Circle in Homewood, California. For the limited purpose of this study, transmitting facilities for those carriers are assumed to be as follows:

| <u>Carrier</u> | <u>Service</u> | <u>Maximum ERP</u> | <u>Antenna Model</u> | <u>Height</u> |
|----------------|----------------|--------------------|----------------------|---------------|
| Carrier #1     | Cellular       | 1,500 watts        | Antel BXA-80040/6    | 110 ft        |
| Carrier #2     | PCS            | 1,500              | Kathrein 742-265     | 75            |
|                | Cellular       | 1,500              |                      |               |

The United States Coast Guard is mounting three Sinclair omnidirectional antennas on the tower, two Model SD214 VHF antennas and one Model SC381 UHF antenna, for transmission at effective heights of 95 and 127 feet above ground, respectively, with a maximum effective radiated power of 560 watts, representing simultaneous operation of four VHF channels at 100 watts each and one UHF channel at 160 watts. The Coast Guard is also installing a receiver-only antenna array at about 143 feet above ground, for direction-finding purposes. There are reported no other wireless telecommunications base stations located nearby.

SBA Network Services, Inc. • New Radio Tower (Site No. CA1142-S)  
Grouse Drive and Chukar Circle • Homewood, California

**Study Results**

For a person anywhere at ground, the maximum cumulative ambient RF exposure level due to the proposed operation of the two carriers is calculated to be 0.016 mW/cm<sup>2</sup>, which is 2.3% of the applicable public exposure limit. The maximum calculated cumulative level at ground, for the simultaneous operation of the carriers and the Coast Guard, is 2.9% of the applicable public limit; the maximum calculated cumulative level at any nearby building\* is 4.4% of the public exposure limit. It should be noted that these results include several “worst-case” assumptions and therefore are expected to overstate actual power density levels.

**No Recommended Mitigation Measures**

Due to their mounting locations, the antennas are not accessible to the general public, and so no mitigation measures are necessary to comply with the FCC public exposure guidelines. It is presumed that the several radio operators will take adequate steps to ensure that their employees or contractors comply with FCC occupational exposure guidelines whenever work is required near the antennas themselves.

**Conclusion**

Based on the information and analysis above, it is the undersigned’s professional opinion that the radio operations proposed at Grouse Drive and Chukar Circle in Homewood, California, will comply with the prevailing standards for limiting public exposure to radio frequency energy and, therefore, will not for this reason cause a significant impact on the environment. The highest calculated level in publicly accessible areas is much less than the prevailing standards allow for exposures of unlimited duration. This finding is consistent with measurements of actual exposure conditions taken at other operating base stations.

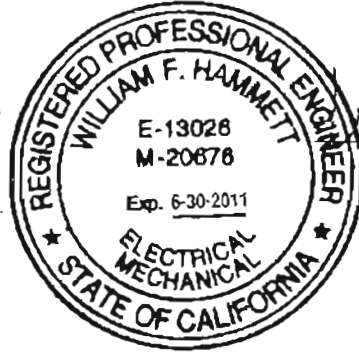
---

\* Located at least 120 feet away, based on aerial photographs from Google Maps.

SBA Network Services, Inc. • New Radio Tower (Site No. CA1142-S)  
Grouse Drive and Chukar Circle • Homewood, California

Authorship

The undersigned author of this statement is a qualified Professional Engineer, holding California Registration Nos. E-13026 and M-20676, which expire on June 30, 2011. This work has been carried out under his direction, and all statements are true and correct of his own knowledge except, where noted, when data has been supplied by others, which data he believes to be correct.



*William F. Hammett*  
William F. Hammett, P.E.

August 24, 2009

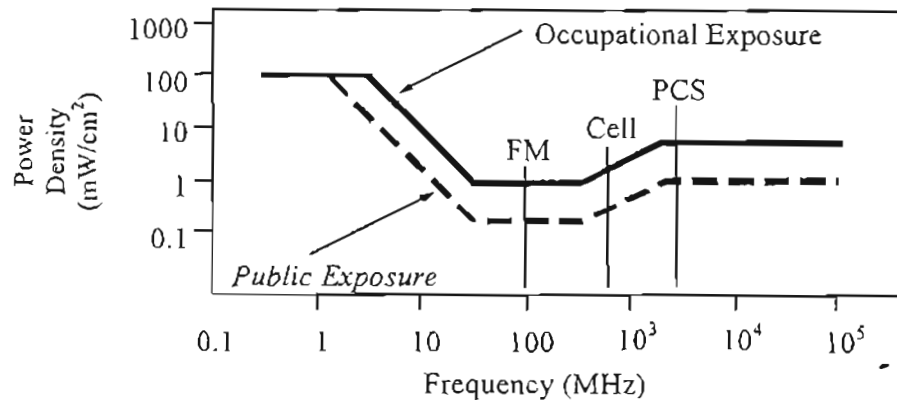


## FCC Radio Frequency Protection Guide

The U.S. Congress required (1996 Telecom Act) the Federal Communications Commission (“FCC”) to adopt a nationwide human exposure standard to ensure that its licensees do not, cumulatively, have a significant impact on the environment. The FCC adopted the limits from Report No. 86, “Biological Effects and Exposure Criteria for Radiofrequency Electromagnetic Fields,” published in 1986 by the Congressionally chartered National Council on Radiation Protection and Measurements (“NCRP”). Separate limits apply for occupational and public exposure conditions, with the latter limits generally five times more restrictive. The more recent standard, developed by the Institute of Electrical and Electronics Engineers and approved as American National Standard ANSI/IEEE C95.1-2006, “Safety Levels with Respect to Human Exposure to Radio Frequency Electromagnetic Fields, 3 kHz to 300 GHz,” includes similar limits. These limits apply for continuous exposures from all sources and are intended to provide a prudent margin of safety for all persons, regardless of age, gender, size, or health.

As shown in the table and chart below, separate limits apply for occupational and public exposure conditions, with the latter limits (in *italics* and/or dashed) up to five times more restrictive:

| Frequency<br>Applicable<br>Range<br>(MHz) | Electromagnetic Fields ( <i>f</i> is frequency of emission in MHz) |                |                                     |               |  |                          |
|---|--|----------------|-------------------------------------|---------------|--|--------------------------|
|   | Electric<br>Field Strength<br>(V/m)                                |                | Magnetic<br>Field Strength<br>(A/m) |               | Equivalent Far-Field<br>Power Density<br>(mW/cm <sup>2</sup> ) |                          |
| 0.3 – 1.34                                | 614  | <i>614</i>     | 1.63                                | <i>1.63</i>   | 100  | <i>100</i>               |
| 1.34 – 3.0                                | 614  | <i>823.8/f</i> | 1.63                                | <i>2.19/f</i> | 100  | <i>180/f<sup>2</sup></i> |
| 3.0 – 30                                  | 1842/f   | <i>823.8/f</i> | 4.89/f                              | <i>2.19/f</i> | 900/f <sup>2</sup>   | <i>180/f<sup>2</sup></i> |
| 30 – 300                                  | 61.4   | <i>27.5</i>    | 0.163                               | <i>0.0729</i> | 1.0  | <i>0.2</i>               |
| 300 – 1,500                               | 3.54√ <i>f</i>   | <i>1.59√f</i>  | √ <i>f</i> /106                     | <i>√f/238</i> | 0/300  | <i>f/1500</i>            |
| 1,500 – 100,000                           | 137  | <i>61.4</i>    | 0.364                               | <i>0.163</i>  | 5.0  | <i>1.0</i>               |



Higher levels are allowed for short periods of time, such that total exposure levels averaged over six or thirty minutes, for occupational or public settings, respectively, do not exceed the limits, and higher levels also are allowed for exposures to small areas, such that the spatially averaged levels do not exceed the limits. However, neither of these allowances is incorporated in the conservative calculation formulas in the FCC Office of Engineering and Technology Bulletin No. 65 (August 1997) for projecting field levels. Hammett & Edison has built those formulas into a proprietary program that calculates, at each location on an arbitrary rectangular grid, the total expected power density from any number of individual radio sources. The program allows for the description of buildings and uneven terrain, if required to obtain more accurate projections.



## RFR.CALC™ Calculation Methodology

### Assessment by Calculation of Compliance with FCC Exposure Guidelines

The U.S. Congress required (1996 Telecom Act) the Federal Communications Commission (“FCC”) to adopt a nationwide human exposure standard to ensure that its licensees do not, cumulatively, have a significant impact on the environment. The maximum permissible exposure limits adopted by the FCC (see Figure 1) apply for continuous exposures from all sources and are intended to provide a prudent margin of safety for all persons, regardless of age, gender, size, or health. Higher levels are allowed for short periods of time, such that total exposure levels averaged over six or thirty minutes, for occupational or public settings, respectively, do not exceed the limits.

#### Near Field.

Prediction methods have been developed for the near field zone of panel (directional) and whip (omnidirectional) antennas, typical at wireless telecommunications base stations, as well as dish (aperture) antennas, typically used for microwave links. The antenna patterns are not fully formed in the near field at these antennas, and the FCC Office of Engineering and Technology Bulletin No. 65 (August 1997) gives suitable formulas for calculating power density within such zones.

For a panel or whip antenna, power density  $S = \frac{180}{\theta_{BW}} \times \frac{0.1 \times P_{net}}{\pi \times D^2 \times h}$ , in mW/cm<sup>2</sup>,

and for an aperture antenna, maximum power density  $S_{max} = \frac{0.1 \times 16 \times \eta \times P_{net}}{\pi \times h^2}$ , in mW/cm<sup>2</sup>,

- where  $\theta_{BW}$  = half-power beamwidth of the antenna, in degrees, and  
 $P_{net}$  = net power input to the antenna, in watts,  
 $D$  = distance from antenna, in meters,  
 $h$  = aperture height of the antenna, in meters, and  
 $\eta$  = aperture efficiency (unitless, typically 0.5-0.8).

The factor of 0.1 in the numerators converts to the desired units of power density.

#### Far Field.

OET-65 gives this formula for calculating power density in the far field of an individual RF source:

$$\text{power density } S = \frac{2.56 \times 1.64 \times 100 \times RFF^2 \times ERP}{4 \times \pi \times D^2}, \text{ in mW/cm}^2,$$

- where ERP = total ERP (all polarizations), in kilowatts,  
RFF = relative field factor at the direction to the actual point of calculation, and  
 $D$  = distance from the center of radiation to the point of calculation, in meters.

The factor of 2.56 accounts for the increase in power density due to ground reflection, assuming a reflection coefficient of 1.6 (1.6 x 1.6 = 2.56). The factor of 1.64 is the gain of a half-wave dipole relative to an isotropic radiator. The factor of 100 in the numerator converts to the desired units of power density. This formula has been built into a proprietary program that calculates, at each location on an arbitrary rectangular grid, the total expected power density from any number of individual radiation sources. The program also allows for the description of uneven terrain in the vicinity, to obtain more accurate projections.

